

Design Calculation of Overlay Laminate for : DN 1200

1. Calculate Axial Loading, Qx :

$$Q_x = \frac{P \times D}{4} \qquad \text{Eq. 8, BS 4994}$$

Where :

$$P = \text{Design pressure} = 1.6 \text{ N/mm}^2$$

$$D = \text{Pipe I.D.} = 1177 \text{ mm}$$

$$Q_x = \frac{1.6 \times 1177}{4}$$

$$Q_x = 470.8 \text{ N/mm}$$

Calculate Design Factor, K

- k1 = 1.5 for hand lay-up
- k2 = 1.2 for long term behavior
- k3 = 1.0 for ambient temp.
- k4 = 1.1 for cyclic stressing
- k5 = 1.1 for post curing procedure

$$K = 3 \times 1.5 \times 1.2 \times 1.0 \times 1.1 \times 1.1 = 6.53$$

Using Design Factor, K = 8

Calculating maximum allowable strain, ϵ

$$\epsilon = \frac{UTUS}{X_z \times K}$$

Where :

- UTUS = Ultimate tensile unit strength, Table 5, BS 4994
- Xz = Unit modulus, Table 5
- K = Design Factor

For Woven Roving, WR :

$$\epsilon = \frac{250}{16000 \times 8}$$

$$\epsilon = 0.0020$$

Take the value for woven roving as the design strain, ϵ_D :

$$\epsilon_D = 0.0020$$

Calculate the Strain-limited allowable loading, U_s for each reinforcement type :

$$U_s = X_z \times \varepsilon_D \times m_z$$

Where :

$$m_z = \text{mass of reinforcement per unit area} = \begin{matrix} 0.270 \text{ kg/m}^2 \text{ for wr270} \\ 0.360 \text{ kg/m}^2 \text{ for wr360} \\ 0.580 \text{ kg/m}^2 \text{ for wr580} \end{matrix}$$

For WR 270:

$$U_s = 16000 \times 0.0020 \times 0.270$$

$$U_s = 8.44 \text{ N/mm}$$

For WR 360 :

$$U_s = 16000 \times 0.0020 \times 0.360$$

$$U_s = 11.25 \text{ N/mm}$$

For WR 580 :

$$U_s = 16000 \times 0.0020 \times 0.580$$

$$U_s = 18.13 \text{ N/mm}$$

2. Determining the number of layers per reinforcement :

$$Q_x \leq (U_s \times n_1)_{270} + (U_s \times n_2)_{360} + (U_s \times n_3)_{580}$$

$$Q_x \leq (8.44 n) + [11.25 (n-1)] + [18.13 (n-2)]$$

$$470.8 \leq 37.81 n - 47.5$$

$$n = 14 \text{ layers wr270}$$

13.70

$$n - 1 = 13 \text{ layers wr360}$$

$$n - 2 = 12 \text{ layers wr580}$$

$$\text{Total layers} = 38 \text{ total layers}$$

3. Calculate thickness of overlay laminate , TLAM :

For WR 270:

$$m_{wr} = 0.270 \times 14$$

$$m_{wr} = 3.70 \text{ kg./m}^2$$

$$t_{270} = m_{wr270} \times t_c$$

where :

$$t_c = \text{thickness constant for "E" glass csm \& wr} = 0.391$$

$$t_c = \text{thickness constant for resin} = 0.769$$

$$t_{270} = 3.70 \times 0.391$$

$$t_{270} = 1.45 \text{ mm}$$

For thickness of resin in wr270 : Assume a 50 : 50 glass : resin ratio

$$m_{resin270} = \frac{m_{wr}}{(100-50)/50}$$

where :
 glass = 50 %
 resin = 50 %

$$m_{resin270} = 3.70 \text{ kg/m}^2$$

$$t_{resin270} = 3.70 \times 0.769$$

$$t_{resin270} = 2.85 \text{ mm.}$$

$$TLAM_{wr 270} = 1.45 + 2.85$$

$$TLAM_{wr 270} = 4.29 \text{ mm.}$$

For WR 360 :

$$m_{wr} = 0.360 \times 13$$

$$m_{wr} = 4.57 \text{ kg./m}^2$$

$$t_{360} = 4.57 \times 0.391$$

$$t_{360} = 1.79 \text{ mm}$$

$$m_{resin360} = 4.57 \text{ kg/m}^2$$

$$t_{resin360} = 4.57 \times 0.769$$

$$t_{resin360} = 3.52 \text{ mm}$$

$$TLAM_{wr 360} = 1.79 + 3.52$$

$$TLAM_{wr 360} = 5.31 \text{ mm}$$

For WR 580 :

$$m_{wr} = 0.580 \times 12$$

$$m_{wr} = 6.79 \text{ kg./m}^2$$

$$t_{580} = 6.79 \times 0.391$$

$$t_{580} = 2.65 \text{ mm}$$

$$m_{resin580} = 6.79 \text{ kg./m}^2$$

$$t_{resin580} = 6.79 \times 0.769$$

$$t_{resin580} = 5.22 \text{ mm}$$

$$\text{TLAMwr 580} = 2.65 + 5.22$$

$$\text{TLAMwr 580} = 7.9 \text{ mm}$$

$$\text{TLAM} = \text{TLAM270} + \text{TLAM360} + \text{TLAM580}$$

$$\text{TLAM} = 4.29 + 5.31 + 7.9$$

$$\text{TLAM} = 17.48 \text{ mm.}$$

To check :

$$Q_x \leq (U_s \times n1)_{270} + (U_s \times n2)_{360} + (U_s \times n3)_{580}$$

$$470.8 \leq 115.65 + 142.95 + 212.19$$

$$470.8 \leq 470.80 \quad \text{Therefore: } \mathbf{OK}$$

4. Calculate the length of overlay laminate, L_j :

$$L_j = \frac{Q_a \times K_{ovl}}{\text{Lap Shear Strength}} \quad \text{Eq. 56, BS 4994}$$

Where :

L_j = Length of joint overlay

Q_a = Q_x = 470.8 N/mm.

K_{ovl} = K = 8

Lap shear Strength : 7

$$L_j = \frac{470.8 \times 8}{7}$$

$$L_j = 539.00 \text{ mm.}$$

Employing the same calculations with the following variables :

DN = Pipe nominal diameter, mm.

I. D. = Pipe internal diameter, mm.

O.D. = Pipe outside diameter, mm.

TLAM = Lamination thickness, mm

L_j = Length of joint lamination, mm.

And the constant value of P = 1.6 N/mm², as Design Pressure:

We have determined TLAM and L_j for the following pipe sizes as shown in Table 2. below:

Table 2. Overlay Laminate minimum widths and thicknesses

Pipe Size DN	I.D. mm.	O.D mm.	TLAM* mm.	Lj mm.	Design t** mm
150	145	157	2.00	67.00	
200	196	208	4.00	90.00	
250	247	259	5.00	113.00	
300	296	310	5.00	136.00	
400	394	412	7.00	181.00	6.66
500	494	514	9.00	226.00	
600	590	616	10.00	270.00	
700	684	718	15.00	313.00	14.04
800	786	820	15.00	360.00	
1000	980	1024	17.00	449.00	
1200	1179	1228	21.00	539.00	14.48
1400	1371	1432	23.00	627.00	20.58
1600	1572	1636	27.00	719.00	24.43
1800	1781	1845	30.00	815.00	
2000	1974	2044	34.00	903.00	

* using csm450 and wr600

** using the wr glass indicated above

5. Determining the mass of laminate materials :

Where :

OD = **1228** mm.

Lj = **539** mm.

Total Mass of Glass Required:

Tmwr = m270 + m360 + m580 kg/m2

= (3.70 + 4.57 + 6.79) x 3.14 (OD + TLAM) x Lj

= 15.07 x 3.14 x 1.25 x 0.539

Tmwr = 31.76 kg.

Since, glass to resin ratio is 50 : 50 by mass :

Tmresin = 31.76 kg.

Therefore, total mass of materials to be used :

Tmass = 63.51 kg.

Prepared by :

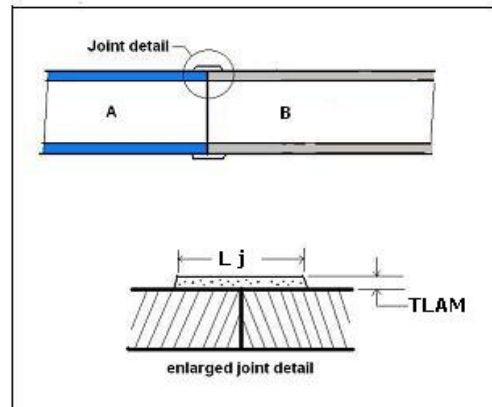


Fig 1. Typical section of butt weld lamination